NOTES:

Exam is 30% of final grade

Open everything Answer all questions

Each question worth 25 points

1) Consider a homogeneous wall, 20 cm thick, constructed of common brick. The wall is initially at a uniform temperature of 20 C. At time t = 0, the outside surface temperture undergoes a step change to 30°C. The temperature remains at 30°C for two hours and then undergoes another step change back to 20°C, where it remains for a long time. The indoor surface temperature is constant at 20 C. Using Duhamel's theorem and the response of a plane wall to a step change in surface temperature, develop an expression for the temperature at the inside surface as a function of time for all times greater than t = 0. The solution should give the temperature in °C as a function of time in seconds. You don't have to actually solve the equation, but you should clearly specify the physical value and engineering units of each variable in the equations and ensure dimensional consistency.

The properties of common brick are as follows.

Density
Conductivity
Specific Heat
Thermal Diffusivity  $C_{p} = 0.84 \text{ kJ/kg C}$ Thermal Diffusivity  $C_{p} = 0.84 \text{ kJ/kg C}$   $C_{p} = 0.84 \text{ kJ/kg C}$   $C_{p} = 5.2 \times 10^{7} \text{ m}^{2}/\text{s}$  L = 0.20 mThermal Diffusivity  $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot 2 \times 10^{7} \text{ m}^{2}/\text{s}$   $C_{p} = \frac{1}{5} \cdot$ 

 $T = T_o + \left(T_{\infty} - T_o\right) \int \left[1 - \left(\frac{x}{L}\right) - Z\right] \sum_{n=1}^{\infty} \frac{\sin n\pi(\frac{x}{L})}{n\pi} e^{-\left(n^2 \pi^2 \frac{x}{L}\right)} t$ 

NOTE THAT (0 X=L T= ZO°C DUE TO BOUNDARY CONDITIONS.

## For t > 2 hours

$$u(x,\theta) = U(x,0) - U(x,\theta-\theta_{1})$$

$$u(x,\theta) = \int_{-\infty}^{\infty} \frac{d}{dt} (7200 \text{ s}) = 0.0936$$

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$$- \left[ 1 - \frac{d}{dt} - Z \sum_{n=1}^{\infty} \frac{\sin(n\pi t t_{n})}{n\pi t} e^{-n^{2}\pi^{2}\theta} - e^{-n^{2}\pi^{2}\theta} \right]$$

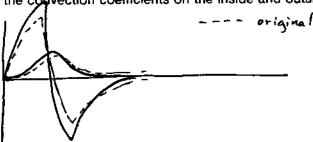
$$= 2 \sum_{n=1}^{\infty} \frac{\sin(n\pi t_{n})}{n\pi t} e^{-n^{2}\pi^{2}\theta} \left( e^{-n^{2}\pi^{2}\theta_{1}} - 1 \right)$$

$$T = T_{0} + \left( T_{0} - T_{0} \right) \left[ Z \sum_{n=1}^{\infty} \frac{\sin(n\pi t_{n})}{n\pi t} - e^{-n^{2}\pi^{2}\theta_{1}} + e^{-n^{2}\pi^{2}\theta_{1}} - 1 \right)$$

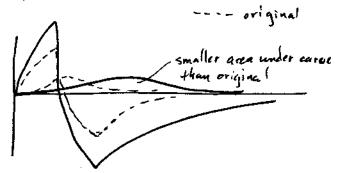
NOTE THAT AT X=L, T = 20°C

2) Figure A shows the heat flux at the indoor and outdoor surface for a 4" insulated frame wall exposed to a 1°C triangular pulse in outdoor temperature with a base of 2 hours. Qualitatively describe the effects on the following changes in wall characteristics.

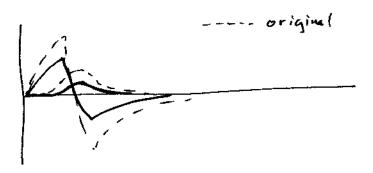
a) Increase the convection coefficients on the inside and outside surfaces.



b) Add a layer of 2 inch face brick on the outside surface.



c) Replace the insulation with material having a lower thermal conductivity.



- 3) Figure A shows the heat flux at the indoor and outdoor surface for a 4" insulated frame wall exposed to a 1°C triangular pulse in outdoor temperature with a base of 2 hours.
  - a) Identify the  $Y_i$  and  $Z_i$  response factors on the figure. SEE FIGURE A.
  - b) The wall, initially at 20°C for t < 0, is exposed to temperature boundary conditions given by the table below. Complete the table by calculating the heat flux.

Time (hr)	Outdoor Temperature (°C)	Indoor Temperature (°C)	indoor Heat Flux (W/m²)
0	20.0	20.0	0.0
1	30.0	20.0	0.6
2	30.0	20.0	1.7
3	20.0	20.0	1.3

a) 
$$Y_{i} = 0.06$$
  $Z_{i} = 0.47$  FOR SYMMETRIC WALL  $Y_{i} = 0.11$   $Z_{i} = -0.26$   $X_{j} = Z_{j}$   $Y_{z} = 0.02$   $Z_{z} = -0.02$ 

b) 
$$q_{i}(t) = \sum_{j=0}^{\infty} Y_{j} T_{o}(t-ja) - \sum_{j=0}^{\infty} Z_{j} T_{i}(t-ja)$$
  
 $T)efine T^{*} = T - 20^{\circ}C$   
 $Q_{i}(t) = \sum_{j=0}^{\infty} Y_{j} T_{o}^{*}(t-ja)$   
 $Q_{i}(1) = Y_{o} \cdot \{T_{o}(1) - 20^{\circ}C\} = 0.06 \cdot 10 = 0.6 \text{ W/m}^{2}$   
 $Q_{i}(z) = Y_{o} \cdot \{T_{o}(z) - 20^{\circ}C\} + Y_{i} \{T_{o}(1) - 20^{\circ}C\}$   
 $= 0.06 \cdot 10 + 0.11 \cdot 10 = 1.7 \text{ W/m}^{2}$   
 $Q_{i}(3) = Y_{o} \cdot \{T_{o}(5) - 20^{\circ}C\} + Y_{i} \{T_{o}(z) - 20^{\circ}C\} + Y_{i} \cdot \{T_{o}(z) - 20^{\circ}C\}$   
 $= 0.06 \cdot 0 + 0.11 \cdot 10 + 0.02 \cdot 10 = 1.3 \text{ W/m}^{2}$ 

4. The heat transfer through a lightweight concrete wall is being analyzed by finite difference methods. At some time  $t = t_0$ , the following temperatures are observed in the wall. (Values of x are given in meters.)

$$T(x=0,t_0) = 24$$
°C  $T(x=0.02,t_0) = 20.8$ °C  $T(x=0.04,t_0) = 22$ °C  $T(x=0.06,t_0) = 24$ °C

If the temperatures at x=0 and x=0.06 are maintained at 24°C, what are the temperatures at the two interior locations at  $t=t_0+5$  minutes?

The properties of the wall are as follows.

Density 
$$f = 1800 \text{ kg/m}^3$$
 $Conductivity$   $f = 1.70 \text{ W/m}^3\text{C}$ 
 $Conductivity$   $f = 1.70 \text{ W/m}^3\text{C}$ 
 $Consider Euler finite difference method. For interior nodes

$$T_m^{pri} = Fo\left(T_{m-1}^p + T_{m+1}^p\right) + \left(1 - 2Fo\right)T_m^p$$

$$Fo = \frac{d}{dx^2} \left(\frac{1}{2}\right)^2 For \text{ STABILITY}$$

$$\Delta t \leq \frac{Dx^2}{2\alpha} \qquad \Delta x = 0.02 \text{ m}$$

$$\delta t \leq \frac{0.0004}{2(1.02U0 \times 10^{-6})} \leq 194.8 \text{ Second s}$$
LET  $\Delta t = 150 \text{ s} = 2\%2 \text{ minutes}$   $Fo = 0.385$$ 

@ 
$$t = t_{0} + 150 s$$
  
 $T'_{1} = F_{0}(T_{0}^{\circ} + T_{2}^{\circ}) + (1 - 2F_{0})T_{1}^{\circ} = 2Z.49 ^{\circ}C$   
 $T'_{2} = F_{0}(T_{1}^{\circ} + T_{3}^{\circ}) + (1 - 2F_{0})T_{2}^{\circ} = 2Z.31 ^{\circ}C$   
@  $t = t_{0} + 300 s$   
 $T'_{1} = F_{0}(T'_{0} + T'_{2}) + (1 - 2F_{0})T'_{1} = 23.00 ^{\circ}C$   
 $T'_{2} = F_{0}(T'_{1} + T'_{3}) + (1 - 2F_{0})T'_{2} = 23.03 ^{\circ}C$ 

## HEAT FLUX AT WALL SURFACE Unit Outdoor Temperature Pulse

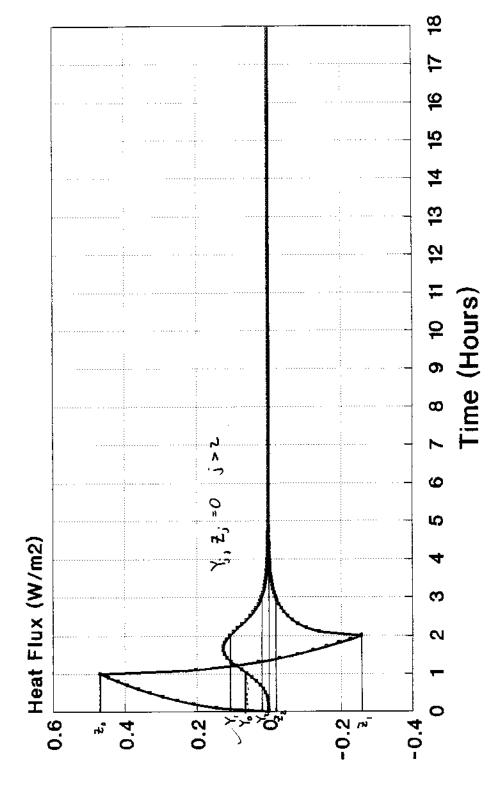


FIGURE A